

Measurement of Interfacial Tension between Methane and Aqueous Solution Containing Hydrate Kinetic Inhibitors

Peng Liu,[†] Chang-Yu Sun,[†] Bao-Zi Peng,[‡] Jun Chen,[‡] and Guang-Jin Chen^{*†}

State Key Laboratory of Heavy Oil Processing, China University of Petroleum, Beijing 102249, PR China, and High Pressure Fluid Phase Behavior & Property Research Laboratory, China University of Petroleum, Beijing 102249, PR China

Interfacial tension of CH₄ + kinetic inhibitors, inhibex 301, and inhibex 501 systems was measured at different concentrations of hydrate inhibitors using the pendant-bubble method. The temperature and pressure ranges were (274.2 to 282.2) K and (0.1 to 20.1) MPa, respectively. The experimental data show that the interfacial tension between methane and aqueous solution of hydrate inhibitor decreases with the increase of pressure and inhibitor concentration. It implied that the interface behavior of inhibex 301 and inhibex 501 is similar to a surfactant. The presence of inhibex 301 in water makes the interfacial tension decrease more remarkably compared with inhibex 501.

Introduction

A hydrate plug often occurs in oil and gas pipelines. Economic and environmental concerns suggested that the low-dosage hydrate inhibitors, including kinetic inhibitors and antiagglomerants, should be selected for solving the question of the hydrate plug.¹ However, the inhibition mechanism of kinetic inhibitors is not very clear yet. The initial hydrate formation usually occurs at the gas–liquid interface.^{2–4} The gas–liquid interfacial tension then plays an important role in hydrate formation processes. The investigation of interfacial tension at the gas–liquid interface is capable of providing information which is helpful in revealing the mechanism of hydrate formation and inhibition. However, interfacial tension data near the hydrate formation conditions are relatively scarce in the literature, especially for methane + water with hydrate kinetic inhibitors. For methane + water, Jho et al.⁵ have reported interfacial tension data at (275.2 to 323.2) K and (0.1 to 6.6) MPa; however, the majority of the literature data^{6–11} has been measured at temperatures above 296 K as Schmidt et al.¹² summarized. In addition, Sun et al.¹³ and Watanabe et al.¹⁴ reported the interfacial tension of methane + water with surfactant near hydrate formation conditions.

In this work, the interfacial tension data between methane and aqueous solution containing kinetic inhibitor, inhibex 301, or inhibex 501 were measured at $T = (274.2 \text{ to } 282.2) \text{ K}$ and $P = (0.1 \text{ to } 20.1) \text{ MPa}$, at four different of inhibitor mass fractions (0.5 %, 1.0 %, 1.5 %, and 2.0 %). The effects of pressure, temperature, and inhibitor mass fraction were examined.

Experimental Section

Apparatus. The JEFRI pendant-bubble high-pressure interfacial tension apparatus manufactured by D.B. Robinson Corporation was used.¹³ The operating temperature was controlled by three Eurotherm temperature controllers with an uncertainty of 0.1 K. All the pressure gauges were calibrated using a standard RUSKA dead-weight pressure gauge with an

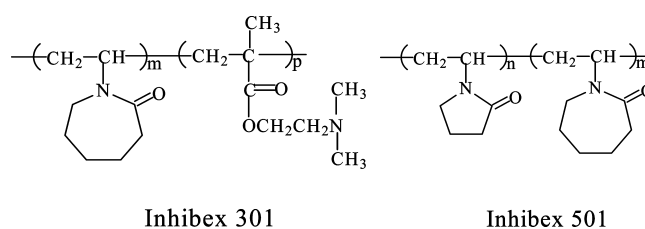


Figure 1. Monomer units for the two hydrate kinetic inhibitors.

uncertainty of 0.25 %. The densities of the aqueous phase containing different mass fractions of inhibitor at ambient temperature and atmospheric pressure were measured by the DMA48 densimeter, manufactured by Anton Paar Corporation, with an uncertainty of $0.001 \text{ g}\cdot\text{cm}^{-3}$. Luo et al.¹⁵ and Sun et al.^{13,16} have used this device to measure the interfacial tension data of the C₂H₄ + water with surfactant system, the CH₄ + water system with surfactant, and the CO₂ + crude oil + reservoir water system, respectively.

Materials. Methane was supplied by the Beijing Analytical Instrument Corporation with a purity of 99.99 %. The water was distilled twice, and the conductivity was less than $10^{-4} \text{ S}\cdot\text{m}^{-1}$. Hydrate kinetic inhibitors (inhibex 301, a 50 % mass fraction solution of the dipolymer of *N*-vinylcaprolactam and dimethylaminoethylmethacrylate in butoxyethanol; inhibex 501, a 50 % mass fraction solution of the dipolymer of *N*-vinylcaprolactam and vinylpyrrolidone in butoxyethanol) were provided by ISP Technologies Inc. The monomer units for the two hydrate kinetic inhibitors are shown in Figure 1.

Experimental Procedure. Experimental procedures have been described in previous papers published by our laboratory.^{13,15,16} Thus only a brief description is given below.

When the system temperature was stable, methane was charged slowly into the pendant-bubble cell through the bottom valve of the cell until the desired pressure was reached. The system was left at the constant temperature and pressure as long as possible for liquid to be saturated with methane gas. A gas bubble was introduced slowly into the pendant-bubble cell through the central injection needle by a JEFRI pump. The gas bubble was swollen to the largest dimension just before it broke,

* Corresponding author. Fax: +86 10 89733252. E-mail: gjchen@cup.edu.cn.

[†] State Key Laboratory of Heavy Oil Processing.

[‡] High Pressure Fluid Phase Behavior & Property Research Laboratory.

Table 1. Densities of Aqueous Solution Containing Different Mass Fractions w of Inhibex 301 and Inhibex 501 at 282.2 K and Atmospheric Pressure

100 w	inhibex 301	inhibex 501
	$\rho/(\text{g}\cdot\text{cm}^{-3})$	$\rho/(\text{g}\cdot\text{cm}^{-3})$
0.5	1.003	1.001
1.0	1.004	1.002
1.5	1.005	1.003
2.0	1.006	1.004

and it was stabilized for about five minutes at the experimental pressure. In this way, the pendant bubble was maintained in physical equilibrium with its surroundings. Then its profile was magnified by the microscope and recorded by a computer through the video camera. The dimensions of the bubble profile could be disposed automatically using software developed by our laboratory.

Calculation of Interfacial Tension. If the bubble is in equilibrium with its surroundings, the interfacial tension (γ) values can be calculated directly from an analysis of the stresses in the static pendant bubble, using the following equations developed by Andreas et al.¹⁷

$$\gamma = \Delta\rho d_e^2 g / H \quad (1)$$

$$1/H = f(d_s/d_e) \quad (2)$$

where $\Delta\rho$ is the density difference between the two phases; d_e is the unmagnified equatorial diameter of the bubble; g is the gravitational constant; d_s is the diameter of the bubble at a selected horizontal plane at height equal to the maximum diameter d_e . Stauffer¹⁸ extended a more detailed table of $1/H$ as a function of d_s/d_e . The Patel-Teja equation of state¹⁹ was used to calculate the density of methane. The correlation of Rowe and Chou²⁰ was used to calculate the density of pure water at different temperature and pressure. For containing low dose of inhibitor system, the density correlated for pure water was modified according to the experimental data at ambient temperature and atmospheric pressure measured by a DMA48 densimeter, which was listed in Table 1. The effect of the solubility of methane on the density of the aqueous phase was negligible because its solubility is very low.²¹

Error Analysis. If defining a parameter $\sigma = d_e^2 g / H$, we can obtain the following formulation from eq 1

$$d\gamma = \left(\frac{\partial\gamma}{\partial\sigma}\right)_{\Delta\rho} d\sigma + \left(\frac{\partial\gamma}{\partial(\Delta\rho)}\right)_{\sigma} d(\Delta\rho) \quad (3)$$

Substituting $(\partial\gamma/\partial\sigma)_{\Delta\rho} = \Delta\rho$ and $(\partial\gamma/\partial(\Delta\rho))_{\sigma} = \sigma$ into eq 3, we get

$$d\gamma = \Delta\rho d\sigma + \sigma d(\Delta\rho) \quad (4)$$

From eq 4 we obtained the following equation for evaluating the uncertainty of the interfacial tension measurement, $\delta\gamma$.

$$\delta\gamma = \Delta\rho\delta\sigma + \sigma\delta(\Delta\rho) \quad (5)$$

where $\delta\sigma$ and $\delta(\Delta\rho)$ denote the uncertainty in measuring and processing the profile of the pendant bubble and that of the density difference resulting from the uncertainties in measuring temperature and pressure, respectively, which are evaluated to be $0.57 \cdot 10^{-6} \text{ N}\cdot\text{m}^2\cdot\text{kg}^{-1}$ and $0.00027 \text{ g}\cdot\text{cm}^{-3}$, respectively. The maximum values of $\Delta\rho$ and σ are $1.006 \text{ g}\cdot\text{cm}^{-3}$ and $63.0 \cdot 10^{-6} \text{ N}\cdot\text{m}^2\cdot\text{kg}^{-1}$, respectively, in this work. The uncertainty of the interfacial tension measurement is therefore determined to be $0.6 \text{ mN}\cdot\text{m}^{-1}$ by using eq 5.

Table 2. Interfacial Tension γ between Methane and Aqueous Solution of Inhibitors Mass Fraction w at $T = 274.2 \text{ K}$

P/MPa	Inhibex 301				Inhibex 501			
	100 w							
	0.5	1.0	1.5	2.0	0.5	1.0	1.5	2.0
	$\gamma/(\text{mN}\cdot\text{m}^{-1})$							
0.1	52.2	50.9	49.3	47.4	62.8	61.3	59.5	57.8
0.9	50.4	49.1	47.5	45.6	60.6	59.3	57.8	56.1
1.7	48.8	47.4	45.6	43.7	58.7	57.3	56.2	54.2
2.5	47.4	45.8	44.2	41.8	57.1	55.7	54.1	52.3
3.3	46.2	44.6	42.6	40.4	55.6	54.1	52.3	50.8
4.1	44.8	43.2	41.2	38.8	54.2	52.4	51.1	49.3
4.9	43.5	41.8	39.9	37.5	52.9	51.2	49.5	47.8
5.7	42.4	40.6	38.7	36.5	51.4	49.9	48.4	46.5
6.5	41.2	39.5	37.3	35.3	49.9	48.6	47.2	45.2
7.3	40.0	38.2	36.2	34.2	48.6	47.3	45.6	44.1
8.1	39.0	37.3	35.2	33.1	47.6	46.3	44.4	43.1
8.9	38.0	36.3	34.5	32.3	46.3	45.1	43.5	42.0
9.7	37.0	35.3	33.6	31.2	45.0	43.8	42.4	41.1
10.1	36.6	34.9	33.2	30.7	44.5	43.2	41.9	40.6
11.1		34.0	32.3	29.5			41.0	39.2
12.1		33.2	31.4	28.8			39.7	38.5
13.1			30.5	28.1			38.6	37.3
14.1			29.4	27.2			37.7	35.9
15.1			28.3	26.2			36.5	35.1
16.1			27.5	25.4			35.3	34.1
17.1			26.7	24.6			34.8	32.9
18.1			26.2	23.8			34.0	32.2
19.1			25.7	23.0			33.0	31.3
20.1			25.2	22.3			32.4	30.8

Table 3. Interfacial Tension γ between Methane and Aqueous Solution of Inhibitors Mass Fraction w at $T = 278.2 \text{ K}$

P/MPa	Inhibex 301				Inhibex 501			
	100 w							
	0.5	1.0	1.5	2.0	0.5	1.0	1.5	2.0
	$\gamma/(\text{mN}\cdot\text{m}^{-1})$							
0.1	50.3	48.4	46.7	45.4	61.0	58.9	57.2	55.7
0.9	48.5	46.8	45.2	43.4	58.9	56.6	55.4	53.8
1.7	47.3	45.2	43.5	41.7	56.9	54.9	53.0	51.7
2.5	45.8	43.9	42.1	40.0	55.4	53.1	51.4	49.7
3.3	44.5	42.6	40.6	38.4	53.7	51.8	50.2	48.3
4.1	43.2	41.3	39.2	36.9	52.4	50.2	48.7	47.0
4.9	41.6	39.9	37.8	35.2	50.9	48.7	47.2	45.9
5.7	40.4	38.6	36.6	33.8	49.5	47.6	46.0	44.5
6.5	39.1	37.2	35.4	32.6	48.2	46.3	44.7	43.1
7.3	37.9	36.1	34.3	31.6	47.0	45.0	43.2	41.8
8.1	36.7	35.0	33.1	30.6	45.8	43.6	42.0	40.4
8.9	35.6	33.7	32.0	29.7	44.5	42.4	40.8	39.2
9.7	34.8	32.7	30.9	28.8	43.2	41.3	39.8	38.2
10.1	34.2	32.3	30.3	28.3	42.8	40.6	39.4	37.7
11.1	33.0	31.2	29.4	27.3			38.4	36.9
12.1	32.0	30.2	28.4	26.2			37.5	35.9
13.1	30.9	29.1	27.4	25.1			36.5	35.0
14.1	29.8	28.2	26.5	24.2			35.8	34.1
15.1			25.7	23.2			34.9	32.8
16.1			24.9	22.3			34.0	31.8
17.1			23.9	21.6			33.4	31.0
18.1			23.1	20.7			32.7	30.6
19.1			22.1	20.0			31.9	29.9
20.1			21.5	19.1			31.2	29.0

Results and Discussion

The experimental method mentioned above was used to measure the interfacial tension of CH_4 + aqueous solution of inhibex 301 and inhibex 501 at different temperatures and pressures under four groups of inhibitor compositions. As hydrate may form in the system studied when the pressure is higher than the equilibria pressure, the measurement of the interfacial tension should be carried out within the induction period of hydrate formation. The experimental results were listed in Tables 2 to 4. As shown in Tables 2 to 4, it can be seen that

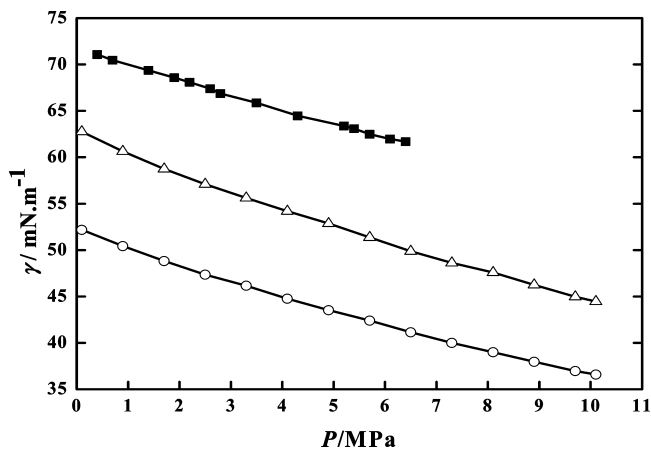


Figure 2. Comparison of interfacial data measured for the methane and aqueous solution system: \circ , $T = 274.2$ K, $w = 0.5$ % inhibex 301; Δ , $T = 274.2$ K, $w = 0.5$ % inhibex 501; \blacksquare , $T = 275.2$ K, pure water (Jho et al.⁵).

Table 4. Interfacial Tension γ between Methane and Aqueous Solution of Inhibitors Mass Fraction w at $T = 282.2$ K

P/MPa	Inhibex 301				Inhibex 501			
	100 w							
	0.5	1.0	1.5	2.0	0.5	1.0	1.5	2.0
	$\gamma/(\text{mN}\cdot\text{m}^{-1})$							
0.1	49.1	47.2	45.6	44.3	58.8	56.4	54.5	53.2
0.9	47.3	45.1	44.1	42.5	56.7	54.4	52.8	51.3
1.7	45.7	43.5	42.4	40.6	55.0	52.8	51.2	49.8
2.5	44.2	42.2	40.8	39.2	53.6	51.2	49.7	48.5
3.3	42.9	40.8	39.1	37.7	52.0	49.8	48.2	46.6
4.1	41.4	39.4	37.4	35.7	50.5	47.9	46.5	44.9
4.9	40.1	37.7	35.7	34.3	49.1	46.7	45.1	43.6
5.7	38.6	36.3	34.2	32.7	47.7	45.4	44.0	42.3
6.5	37.2	35.0	33.1	31.0	46.3	44.2	42.4	41.0
7.3	35.9	33.8	31.6	29.6	45.0	42.8	41.3	39.6
8.1	34.6	32.5	30.3	28.3	43.8	41.5	39.8	38.2
8.9	33.6	31.3	29.1	27.1	42.6	40.3	38.7	37.0
9.7	32.4	30.2	28.1	25.8	41.3	39.4	37.7	35.9
10.1	31.9	29.7	27.7	25.5	40.7	38.9	37.3	35.6
11.1	30.8	28.7	26.7	24.3			36.5	34.3
12.1	29.7	27.5	25.5	23.2			35.7	33.2
13.1	28.5	26.4	24.4	22.3			34.9	32.4
14.1			23.6	21.4			33.9	31.8
15.1			22.6	20.5			33.2	31.0
16.1			21.8	19.7			32.5	30.1
17.1			20.8	18.7			31.9	28.9
18.1			19.8	18.0			31.2	28.2
19.1			19.2	17.3			30.5	27.4
20.1			18.4	16.5			29.6	26.9

the interfacial tension of CH_4 + aqueous solution of inhibitors decreases with the increase of pressure and the mass fraction of hydrate inhibitors at fixed temperature. The interfacial tension also slightly decreases with an increase in temperature.

Figure 2 shows the comparison of the interfacial tension data of the methane and aqueous solution system as a function of pressure measured in this work with that reported by Jho et al.⁵ at the approximate temperature. Compared with the pure water system, adding inhibex 301 or inhibex 501 to water, the interfacial tension between methane and the aqueous solution decreases. This implied that the methane adsorption on the gas–liquid interface was more significant in aqueous solution of inhibitors than in pure water. Figure 3 also shows the variation of interfacial tension data at different inhibitor mass fractions at 278.2 K and 0.1 MPa. It could be seen that the interfacial tension decreases sharply with the addition of inhibitor, especially inhibex 301. It is known that butoxyethanol is contained in these two inhibitors. In general, adding a certain

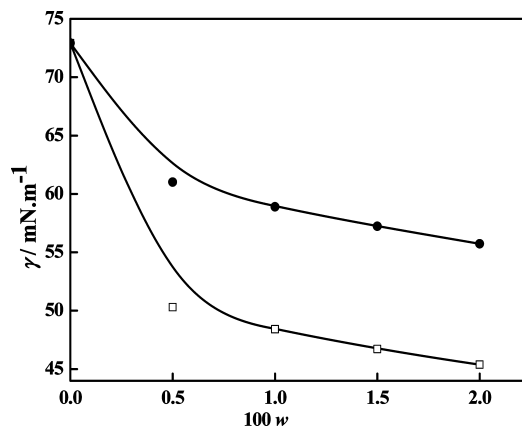


Figure 3. Interfacial tension as a function of inhibitor mass fraction w at $T = 278.2$ K and $P = 0.1$ MPa: \square , inhibex 301; \bullet , inhibex 501.

amount of butoxyethanol to water can also decrease the interfacial tension. However, the concentration of butoxyethanol in this work is not sufficient for such a substantial reduction of interfacial tension.²² Therefore, the substantial reduction of interfacial tension is attributed mainly to inhibex 301 or inhibex 501. With the increased inhibitor mass fraction in water, the interfacial tension decreases slowly. This is similar to the relation of interfacial tension and the concentration of surfactants in water. Therefore, we think that the interface behavior of inhibex 301 or inhibex 501 is similar to a surfactant.

Literature Cited

- Zanota, M. L.; Dicharry, C.; Graciaa, A. Hydrate Plug Prevention by Quaternary Ammonium Salts. *Energy Fuels* **2005**, *19*, 584–590.
- Peng, B. Z.; Dandekar, A.; Sun, C. Y.; Luo, H.; Ma, Q. L.; Pang, W. X.; Chen, G. J. Hydrate Film Growth on the Surface of a Gas Bubble Suspended in Water. *J. Phys. Chem. B* **2007**, *111*, 12485–12493.
- Ohmura, R.; Matsuda, S.; Uchida, T.; Ebinuma, T.; Narita, H. Clathrate Hydrate Crystal Growth in Liquid Water Saturated with a Guest Substance: Observations in a Methane + Water System. *Cryst. Growth Des.* **2005**, *5*, 953–957.
- Taylor, C. J. K.; Miller, T. C.; Koh, A.; Sloan, E. D., Jr. Macroscopic Investigation of Hydrate Film Growth at the Hydrocarbon/Water Interface. *Chem. Eng. Sci.* **2007**, *62*, 6524–6533.
- Jho, C.; Nealon, D.; Shogbola, S.; King, A. D., Jr. Effect of Pressure on the Surface Tension of Water: Adsorption of Hydrocarbon Gases and Carbon Dioxide on Water at Temperatures between 0 and 50°C. *J. Colloid Interface Sci.* **1978**, *65*, 141–154.
- Hough, E. W.; Rzasca, M. J.; Wood, B. B. Interfacial Tensions at Reservoir Pressures and Temperatures; Apparatus and the Water–Methane System. AIMME Tech. Paper 3019. *J. Petrol. Technol.* **1951**, *3* (2), 57–60.
- Slowinski, E. J.; Gates, E. E.; Waring, C. E. The Effect of Pressure on the Surface Tensions of Liquids. *J. Phys. Chem.* **1957**, *61*, 808–810.
- Jennings, H. Y., Jr.; Newman, G. H. The Effect of Temperature and Pressure on the Interfacial Tension of Water against Methane–Normal Decane Mixtures. *Soc. Petrol. Eng. J.* **1971**, *11*, 171–175.
- Massoudi, R.; King, A. D., Jr. Effect of Pressure on the Surface Tension of Aqueous Solutions. Adsorption of Hydrocarbon Gases, Carbon Dioxide, and Nitrous Oxide on Aqueous Solutions of Sodium Chloride and Tetrabutylammonium Bromide at 25 °C. *J. Phys. Chem.* **1975**, *79*, 1670–1675.
- Wiegand, G.; Franck, E. U. Interfacial Tension between Water and Non-polar Fluids up to 473 K and 2800 bar. *Bunsen Phys. Chem.* **1994**, *98*, 809–817.
- Sachs, W.; Meyn, V. Pressure and Temperature Dependence of the Surface Tension in the System Natural Gas/Water Principles of Investigation and the First Precise Experimental Data for Pure Methane/Water at 25 °C up to 46.8 MPa. *Colloids Surf., A* **1995**, *94*, 291–301.
- Schmidt, K. A. G.; Folas, G. K.; Kvamme, B. Calculation of the Interfacial Tension of the Methane–Water System with the Linear Gradient Theory. *Fluid Phase Equilib.* **2007**, *261*, 230–237.

- (13) Sun, C. Y.; Chen, G. J.; Yang, L. Y. Interfacial Tension of Methane + Water with Surfactant near the Hydrate Formation Conditions. *J. Chem. Eng. Data* **2004**, *49*, 1023–1025.
- (14) Watanabe, K.; Niwa, S.; Mori, Y. H. Surface Tensions of Aqueous Solutions of Sodium Alkyl Sulfates in Contact with Methane under Hydrate-Forming Conditions. *J. Chem. Eng. Data* **2005**, *50*, 1672–1676.
- (15) Luo, H.; Sun, C. Y.; Huang, Q.; Peng, B. Z.; Chen, G. J. Interfacial Tension of Ethylene and Aqueous Solution of Sodium Dodecyl Sulfate (SDS) in or near Hydrate Formation Region. *J. Colloid Interface Sci.* **2006**, *297*, 266–270.
- (16) Sun, C. Y.; Chen, G. J. Measurement of Interfacial Tension for the CO₂ Injected Crude Oil + Reservoir Water System. *J. Chem. Eng. Data* **2005**, *50*, 936–938.
- (17) Andreas, J. M.; Hauser, E. A.; Tucker, W. B. Boundary Tension by Pendant Drops. *J. Phys. Chem.* **1938**, *42*, 1001–1019.
- (18) Stauffer, C. E. The Measurement of Surface Tension by the Pendant Drop Technique. *J. Phys. Chem.* **1965**, *69*, 1933–1938.
- (19) Patel, N. C.; Teja, A. S. A New Cubic Equation of State for Fluids and Fluid Mixtures. *Chem. Eng. Sci.* **1982**, *37*, 463–473.
- (20) Rowe, A. M.; Chou, J. C. S. Pressure-volume-temperature-concentration Relation of Aqueous Sodium Chloride Solutions. *J. Chem. Eng. Data* **1970**, *15*, 61–66.
- (21) Peng, B. Z.; Chen, G. J.; Luo, H.; Sun, C. Y. Solubility Measurement of Methane in Aqueous Solution of Sodium Dodecyl Sulfate at Ambient Temperature and near Hydrate Conditions. *J. Colloid Interface Sci.* **2006**, *304*, 558–561.
- (22) Elizalde, F.; Gracia, J.; Costas, M. Effect of Aggregates in Bulk and Surface Properties. Surface Tension, Foam Stability, and Heat Capacities for 2-Butoxyethanol + Water. *J. Phys. Chem.* **1988**, *92*, 3565–3568.

Received for review December 3, 2008. Accepted March 9, 2009. Financial support received from the National Nature Science Foundation of China (Nos. 20676145, U0633003), National 863, NCET-05-0107, and NCET-07-0842 is gratefully acknowledged.

JE800937U